

REMARKS

The specification of the subject U.S. patent application, as filed, as constituted by the verified translation of PCT/DE2003/002348, has been cancelled in favor of the concurrently presented Substitute Specification. A suitable Abstract of the Disclosure has been added. These changes and additions do not constitute any new matter.

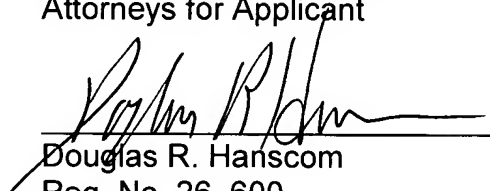
Original claims 1-38, as set forth in the verified translation of PCT/DE2003/002348 have been cancelled and new claims 39-76 have been added. New claims 39-76 are essentially the same, in scope as the claims now pending in the subject PCT application. They have been rewritten in a form more in accordance with U.S. practice and eliminating multiple dependencies.

Entry of this Preliminary Amendment into the file of the subject U.S. patent application, prior to the calculation of the filing fee, and prior to an examination of the application on the merits is respectfully requested.

Respectfully submitted,

Heinrich FEHREN et al.
Applicant

JONES, TULLAR & COOPER, P.C.
Attorneys for Applicant



Douglas R. Hanscom
Reg. No. 26, 600

January 18, 2005
JONES, TULLAR & COOPER, P.C.
P.O. Box 2266 Eads Station
Arlington, Virginia 22202
(703) 415-1500
Attorney Docket: W1.2015 PCT-US

[WO 2004/016431]

[PCT/DE2003/002348]

DT09 Rec'd PCT/PTO 1.8 JAN 2005
MARKED UP COPY OF SPECIFICATIONFEHREN ET AL.: W1.2015 PCT-US

**METHOD AND DEVICE FOR REDUCING VIBRATIONS ON ROTATING PARTS,
AND VIBRATION-DAMPED ROTATING PART**

CROSS-REFERENCE TO RELATED APPLICATIONS

[001] This U.S. Patent Application is the U.S. National Phase, under 35
USC 371, of PCT/DE2003/002348, filed July 12, 2003; published as WO
2004/016431 A1 on February 26, 2004 and claiming priority to DE 102 33 086,
filed July 19, 2002 and to DE 102 53 997, filed November 19, 2002, the
disclosures of which are expressly incorporated herein by reference.

FIELD OF THE INVENTION

[002] The present invention is directed[relates] to a method and to a
device for reducing vibrations of rotating components, as well as to a vibration-
damped rotating component[in accordance with the preambles of claims 1, 9 or
28]. The rotating components roll off against each other. At least one raised area
projects from a substantially circular contour of an effective surface area of at least
one of the rotating components.

BACKGROUND OF THE INVENTION

[003] EP 0 194 618 B1 discloses a device for reducing vibrations which are caused by rolling over a groove located on the surface area. A raise in height of the circular contour for affecting the force change behavior, is provided in this device[here] in the entry or exit area of the groove.

[004] A method for compensating for vibrations of rotating components is disclosed in WO 01/50035 A1. An[, wherein an] actuator is arranged in the area of the surface of the rotating component, which actuator counteracts the vibration by the provision[means] of a force component in the axial direction when the actuator[it] is activated as a function of an[the] angle of rotation position of the rotating component.

SUMMARY OF THE INVENTION

[005] The object of the present invention is directed to providing[based on creating] a method and a device for reducing vibrations of rotating components, as

well as to providing a vibration damped component.

[006] In accordance with the present invention, this object is attained by the provision of at least one raised area projecting from a substantially circular contour of an effective surface area of at least one of two rotating components that roll off on each other. A height of the raised area, in the radial direction, and a position of the raised area, in the circumferential direction, can be changed as a function of a value that defines a printing press status or vibration[means of the characterizing portions of claims 1, 9 or 28].

[007] The advantages to be gained by [means of] the present invention lie, in particular, in that a possibility for effectively and variably reducing vibrations has been provided[created]. The reduction of the vibrations can take place actively, and possibly adaptively, during a production run and can be matched to the operating requirements.

[008] The method and the device in accordance with the present invention can be employed with particular advantage in connection with at least one of two components rolling off on one another, such components being, for example,

cylinders or rollers in which[wherein], viewed in the circumferential direction, at least one of the components has at least one interruption, such as, for example a groove, on its surface area.

[009] Because[By means] of the ability to change, and in particular because of the ability to change, by remote control, the geometry and/or the position and/or the height of the raised area or areas[(s)] on the cylinder surface area, the vibration can optimally be [optimally] reduced through[via] the various operational states, such as the speed of rotation, for example, on the one hand. On the other hand, the geometry and/or the position or the height per revolution, or during a part of the revolution, can be changed or can be modulated in order to do justice to the roll-over of the interruption at each nip point, for example in connection with the contact of the rotating body with several other cylinders and/or rollers.

[010] In an advantageous embodiment of the present invention, an actuator, which can be remotely controlled, is configured[designed] as an actuator which can be charged with a pressure medium, such as, for example, as a

hydraulic or as a pneumatic unit. In a variation, the actuator can be[it is designed]
piezo- electrically configured.

BRIEF DESCRIPTION OF THE DRAWINGS

[011] Preferred[Exemplary] embodiments of the present invention are represented in the drawings and will be described in greater detail in what follows.

[012] Shown are in:

Fig. 1, a schematic depiction[basic sketch] of two rotating components working together, in

Fig. 2, an enlarged representation of a nip point between the two rotating components depicted in [accordance with] Fig. 1, in

Fig. 3, qualitative courses of an acceleration as a function of time, and showing at [(A: vibration without the formation of a raised area, and at B: with the formation of a raised area)], in

Fig. 4, a first preferred[exemplary] embodiment of a[the] device for reducing vibrations in accordance with the present invention, in

Fig. 5, a first preferred[exemplary] embodiment of the integration of a clamping or bracing device, in

Fig. 6, a second preferred[exemplary] embodiment of the integration of a clamping or bracing device, in

Fig. 7, a third preferred[exemplary] embodiment of the integration of a clamping or bracing device, in

Fig. 8, a schematic representation of a[the] method for controlling the device in accordance with the present invention, in

Fig. 9, a qualitative representation of the interrelationship between a roll-off speed and a[the] height of the raised area, or of the pressure, in

Fig. 10, a schematic representation of a[the] method for regulating the device, in

Fig. 11, a qualitative representation of an[the] interrelationship between a relative amplitude and the height of the raised area, or of the pressure, and in

Fig. 12, a schematic representation of a[the] method for regulating

a[the] device with four rotating components acting together respectively in pairs.

DESCRIPTION OF THE PREFERRED EMBODIMENT

[013] Referring initially to Figs. 1 and 2 there is schematically depicted a[A] rotating component 01, for example a cylinder 01, or a roller 01 of a machine, such as, for example, a treatment or a processing machine for webs and sheets, and in particular a cylinder or a roller of a rotary printing press. The cylinder 01 or roller 01[,] cooperates, in a[the] contact position AN₁ with a second rotating component 02, for example a cylinder 02 or a roller 02. The two components 01, 02, called cylinders 01, 02 in the discussion which[what] follows, roll off on or against each other in the area of their effective surface areas 03, 04 and have been placed against each other in a[the] contact position AN, and with a force which, for example, can be predetermined or set, all as seen in [(Fig. 1)]. In an advantageous manner, the present invention can also be applied to rollers and cylinders of similar machinery for producing web-shaped material, such as, for example paper or sheet metal, and the like[etc.], in impression cylinders or in

rolling mills.

[014] At least one of the cylinders 01, 02, such as₁[here] for example the first cylinder 01, configured[designed] as a transfer cylinder 01₁ has, in the area of its effective surface area 03, at least one axially extending interruption 06 of a circumferential surface contour which otherwise is circular in an[the] unstressed state. The interruption 06 is₁ for example₁ based on a joint formed by[of] ends of one or of several dressings 07 that are arranged on the cylinder 01. Alternatively, interruption 06 is caused because[, or in that] the ends of one or of several dressings 07 are arranged in a groove 08 that is extending in an area close to the surface of the cylinder 01. An opening from the surface area of the cylinder 01 to the groove 08 is kept as small as possible, and₁ in an advantageous embodiment₁ such a groove 08 is maximally 3 mm in circumferential width. The groove 08 can widen or open toward the cylinder interior and can have in it a device 10 for clamping and/or for bracing, as seen in [(Fig. 4)]. However, the interruption[it] can also be designed solely as a slit 08.

[015] In the contact position AN, as depicted schematically in Fig. 1, the two cylinders 01, 02 are placed against each other with a force which is greater than zero, and, in the course of the passage of the interruption 06 through the nip point, the two cylinders 01, 02[they] undergo a relief as well as a subsequent renewed stress. A vibration of the cylinder 01, 02, or of the cylinders 01, 02, is excited or caused by this cyclical stress and relief which vibration is, inter alia, a function of the cylinder contact forces, the geometry of the interruptions 06 and the cylinders 01, 02, the properties of the cylinder material, and the number of revolutions, or of[off] a roll- off speed "v." Such a vibration[, curve A,] is qualitatively represented in Fig. 3 as curve or line A, wherein the [dashed] area within the dashed lines identifies the passage of the interruption 06 through the nip point. This vibration, which is excited by the passage of the interruption[(s)] 06, has been damped and should not be confused, at this point, with other vibrations that are possibly induced in the individual cylinders 01, 02 by balance errors, or with a bending caused by gravity and/or the line force. The vibration depicted in Fig. 4 is excited during each[per] revolution of the cylinder 01, 02 in the

circumferential direction in response to alignment of the[once per] interruption 06 and the nip point.

[016] To dampen[For damping] the vibration, at least one of the cylinders 01, 02, [here] for example the cylinder 02 which is configured[designed] as a forme cylinder 02, has at least one axially extending raised area 09 of a cylinder circumferential and axial surface contour, which otherwise is circular in the unstressed state, in the area of its effective surface area 04. This raised area 09 can extend axially continuously over a length of the effective barrel of cylinder 02, or can also extend in one or in several cylinder sections in the axial direction. As indicated in Fig. 2, the raised area 09 has a height h_{09} , depicted as [(the maximum)] weight, in respect to the undisturbed contour or surface of cylinder 02, and an effective distance a_{09} , again depicted as [(the maximum)] distance from the interruption 06 on the cooperating cylinder 01 in relation to a roll-off path at the rotating cylinders 01, 02.

[017] Viewing the passage of the raised area 09, by itself, through the nip point, a vibration is also induced in the cylinders 01, 02 rolling off on each other.

Depending on the relative position in respect to the passage over the interruption 06[09], i.e. depending on the rolled-off distance a09 or [(phase relation)], and the height h09, and/or the shape of the raised area 09, this counter- vibration causes an increase or decrease, and [(in the ideal case, effects a cancellation)] of the vibration amplitude caused by the passage of the interruption 06[09]. Depending on its shape and its position, the raised area 09 provides a support effect between the cylinders 01, 02, which cylinders are radially moved with[in] respect to each other by the excitation.

[018] The height and the shape of the generated counter-vibration is partially a function of the shape of the raised area 09 and₁[-] in case of a raised area 09 having an asymmetrical shape with[in] respect to the circumferential direction, is also partially[-] a function of the direction of rotation of the cylinders 01, 02 rolling off on each other. A course of the resultant curve B of the vibration, caused by the superimposition of the vibration and counter-vibration is represented in Fig. 3, wherein the excitation was generated by the raised area 09 in the form of a ramp, as will be discussed [(see] below[)]. An increase in an[the]

amplitude of the acceleration, which can initially be detected in the area of the passage of the interruption 06[09], which initially can be detected in the area of the passage of the interruption 06[09], is already followed by a clear decrease in the second period. Since the area of the interruption 06[09] is a non-printing area, the brief increase of the resultant vibration does not have a negative effect on the printed image, but the subsequent decrease has a positive effect.

[019] The raised area 09 is now configured[designed] in such a way that its height a09 can be changed with[in] respect to the undisturbed cylinder surface contour, in particular during [the] operation of the cylinder pair 01, 02, i.e. during the roll-off of the cylinders 01, 02. To this end, the cylinder 02 has an actuating assembly[means] 11 for use in changing the height h09, for example an actuating device[means] 11, and in particular a remotely controllable actuator 11. In an advantageous embodiment of the present invention, the circumferential distance a09, as depicted in [(Fig. 4)] is also configured[designed] to be changeable.

[020] The provision of the raised area 09 can be technically realized in various ways. It is thus possible, for example, for fingers, which have been given

a suitable shape, to be sunk₁ in a comb- like manner₁ into recesses in the surface area of the base body of the cylinders 01, 02, and for such fingers to be radially movable₁ by linear or by rotatory movements via an actuating assembly[means]

11. A variation is also possible, in which[wherein] an area of the surface 03, 04 of the respective cylinder 01, 02 has been structured[designed] to be elastically deformable or to be elastically resilient₁ within defined limits₁ and to be deflectable in the radial direction by an actuating assembly[means] 11, such as, for example, cams or an eccentric shaft, or by other actuators, which may be arranged in the interior of the cylinder.

[021] The actuator 11, or the actuators 11, can also be structured[designed] in different ways, for example as a function of the configuration[design] of the raised area 09[are]. It can be configured[designed] as a part of a motor-driven, as a hydraulically or a pneumatically driven unit, or as a unit that operates based on magnetic or on piezo-electric forces.

[022] In the following preferred[exemplary] embodiments, as depicted in [(]Figs. 4 to 12[)], the device and the method in accordance with the present

invention are represented by [means of] the example of a raised area 09 structured[designed] as a tongue, a[/]_lip[/]_or as a[/]_bracket 09, which can be substantially bent[, reversibly springing back,] out of the contour of the surface area 03, 04 of the respective cylinder 01, 02 and which can reversibly spring back into alignment with the contour of the surface area 03, 04. The actuator[activator] 11 activating[actuating] the tongue/lip/bracket 09 has been configured[designed] here as a part of a hydraulically operating unit.

[023] In Fig. 4, the cylinder 02, here provided as a[the] forme cylinder 02, and working together with the transfer cylinder 01, has the tongue/lip/bracket 09, which can be raised. The tongue/lip/bracket 09, which is in the form of a one-armed lever, is embodied by a groove 12, which groove 12 is axially extending inside of the surface area 04 of cylinder 02, and an interruption or cut or opening13 of the surface area[,] connecting the groove 12 with its surroundings. Interruption 13 may be, for example, in the form of an axial cut 13. The tongue/lip/bracket 09 can be raised by the operation[means] of a suitable hydraulic unit, which has [as] an actuator 11 in the form of a reversibly deformable hollow

body 11, which body 11 can be charged with a pressure medium. The actuator 11 is situated[,] in the groove 12 [axially] extending axially in the cylinder 02. The hollow body 11 is arranged directly underneath the tongue/lip/bracket 09 in the interior of the cylinder 02, as is shown in Fig. 4, and is supported₁ toward the interior of cylinder 02, in the radial direction₁ at least partially on a cylindrical face 14[,]₁ which is fixed in place on the cylinder.

[024] Also represented in Fig. 4 is the effective distance a_{09} between the maximum raised area 09, configured [(]here as the edge of the cut or opening 13[)] and the interruption 06 on cylinder 03, as well as an effective length l_{09} of the leg of the tongue/lip/bracket 09. The effective leg length l_{09} of the one-armed lever 09 represents the length of the tongue/lip/bracket 09₁ in the circumferential direction of cylinder 02 from the edge of the cut 13 to the point at which the tongue/lip/bracket 09 is "undermined" by the groove 12, as viewed in the radial direction. In an advantageous embodiment, the tongue/lip/bracket 09 extends over the entire axial length of a barrel of the cylinder 02. In Fig. 4, the tongue/lip/bracket 09 is represented in an active position, i.e. the actuator 11 is

effective or is actuated. In another embodiment of the present invention, with several staggered cylinder grooves, or with several dressings, in which[i.e.] several interruptions 06 that are arranged side-by-side in the axial direction of the cylinder 01 are arranged offset in respect to each other in the circumferential direction, several of the raised areas 09 can be arranged staggered on cylinder 02 in the same way.

[025] The actuator 11, which may be embodied as a hollow body 11, receives its fluid, or its other suitable operating[the] pressure P, from the outside of cylinder 01, for example via a rotary throughput, which is not specifically represented, in the area of a journal, also not specifically represented, of the cylinder 02[03].

[026] When they are placed against each other, the forme cylinder 02 acts together with the transfer cylinder 01, on whose surface a[the] dressing 07, such as, for example, a rubber blanket 07, has been secured or braced. Ends 16, 17 of a[the] single dressing 07, or of two dressings 07 that are arranged one behind the other in the circumferential direction of cylinder 01, are retained[maintained] by the

provision and the use[means] of a clamping and/or a bracing device that is located in the groove 08. The interruption 06 in the effective surface area 03 of the cylinder 01 is formed in the area where the dressing end or ends 16, 17 leave the opening of the groove 08.

[027] In an advantageous embodiment of the invention, the circumferential offset distance a09 is a length corresponding to a path of a sector of the cylinder 01, 02 of an opening angle of -1 to 8°, and in particular of 3° to 6°, on the surface area 03.

[028] In an advantageous embodiment of the present invention, and with cylinders 01, 02 of an axial[a] length l01, l02 of 1,350 to 1,550 mm, and with an effective circumference of 420 to 700 mm, and in particular of 500 to 600 mm, the tongue/lip/bracket 09 has an effective leg length l09 of 10 to 30 mm, and in particular has a length of 16 to 21 mm. The circumferential offset distance a09 is, for example, from 1.25 to 15 mm, and in particular is from 4 mm to 10 mm.

[029] The ratio between the offset distance a09 and the length of the cylinder circumference lies between 0.002 and 0.02, and in particular lies

between 0.005 and 0.015. The ratio between the leg length l09 and the length of the cylinder circumference lies between 0.02 and 0.04, and in particular lies between 0.03 and 0.035.

[030] The raised area 09, configured[designed] as a tongue/lip/bracket 09 in accordance with Fig. 4, has been made asymmetric with[in] respect to the direction of rotation of the cylinder 01, 02, or of the cylinders 01, 02. In one direction of cylinder rotation, the raised area 09[03] acts with[in] a ramp shape and with a correspondingly shaped impulse, while in the other direction of cylinder rotation this raised area 09 acts as an impulse that is induced at a discontinuous skip location. Both forms will exhibit[show] the above described vibration damping or counteracting effect wherein, however, the excitation resultant with travel of the cylinder 01 over the ramp in[/]the direction of rotation, and with a discontinuous skip location, is of greater advantage.

[031] The height h09 and/or the distance a09 can be set differently, depending on the direction of rotation, on the number of rotations and on the force of the contact, or the [()linear force], between the cylinders 01, 02. For this

purpose, it is possible to supply the direction of rotation as a value "g" defining the printing press status or the printing press to a control or regulating device explained further [down] below.

[032] A raised area 09, corresponding to, or similar to the arrangement represented in Fig. 4, by way of example by the forme cylinder 02, can be arranged on the transfer cylinder 01, either additionally to, or in place of the forme cylinder 02. Different variations for integrating a clamping device for the dressing 07, or for its ends 16, 17, are represented in subsequent Figs. 5 to 7. These arrangements can be applied to dressings 07 which may be embodied as printing formes 07 on the forme cylinder 02, or which may be embodied as rubber blankets 07 on the transfer cylinder 01. In the case of rubber blankets 07, the use of metallic printing blankets 07 including an [(elastically deformable layer on a metal support)], is advantageous, since these blankets can be configured[designed] in the area of their ends, similar to those of printing formes 07 and can be clamped in the groove 08.

[033] In Fig. 5, the cut, or opening or interruption 13 is embodied as an

opening 13 in such a way that it has been made very narrow, less than or equal to 3 mm, wherein the ends 16, 17, for example the dressing ends 16, 17, are merely suspended.

[034] In Fig. 6, the cut or opening or interruption 13 is embodied as an opening 13 in such a way that the actuator 11 simultaneously acts on one or on two dressing ends 16, 17, either via a lever mechanism 20, which is [(only schematically indicated)], or directly, and clamps the two dressing ends 16, 17 [them].

[035] In Fig. 7, the cut or opening or interruption 13 is embodied as an opening 13 in such a way that, for example, the leading dressing end 16 is substantially held in place by the shape of the edge. The[, and the] trailing dressing end 17 is clamped by the actuator 11.

[036] As has been discussed in detail[explained] above, the height h09 of the raised area 09 is adapted[made] to be changeable. Preferred[Exemplary] embodiments of a[the] method for controlling or regulating this height h09, and the device required to accomplish such a method[therefore], will be explained in what

follows.

[037] In a first preferred[exemplary] embodiment, as depicted schematically in [(Fig. 8)], the regulation[reduction] takes place by the utilization[means] of a control system, which control system can contain a lower order regulating circuit.

[038] A value "v" defining the printing press status, and in particular defining the roll-off speed "v," such as the number of revolutions or the angular speed, for example, is used as the command variable of the higher order control system. This value "v" can be obtained, for example, together with other values "g" defining the printing press status or the printing press, from a higher order printing press control device, or can also be measured in a suitable manner. Now, a reference variable of the manipulated variable is assigned to the value "v" in a logical unit 18 by the use[means] of a stored interrelationship, such as, for example [(by the use[means] of a table, arithmetically, or the like[etc.])] as the output value of the logical unit 18. The manipulated variable can directly be a desired height h_{09} of the raised area 09, a pressure P , a distance S , a voltage U ,

or the like[etc]. Accordingly, a reference variable h_{09_SOLL} for the height h_{09} of the raised area 09, a reference variable P_{SOLL} for the pressure P of a hydraulic unit, a reference variable S_{SOLL} for a travel or position signal S of an actuator 11, or a reference variable U_{SOLL} for the voltage signal U of an actuator 11, are determined as the output values. This reference variable h_{09_SOLL} , P_{SOLL} , S_{SOLL} , U_{SOLL} , is again used as a command variable for a lower order regulator device 19. A regulating device 21, for example a regulator 21, and in particular a controlled system 22 of the regulating device 21, can now be embodied in different ways, and can be matched to the type of the actuator 11 and to the input values.

[039] A functional, or an algebraic, and in particular a linear interrelationship between the roll-off speed "v" and the desired raised area 09 [(]or of an appropriate travel, pressure or voltage signal[)] has been stored in the logical unit 18 as the logic. This [(in particular linearized)] interrelationship, which is particularly linearized, between the roll-off speed "v" and the reference variable h_{09_SOLL} , P_{SOLL} , S_{SOLL} , U_{SOLL} for the height h_{09} of the raised area 09, or the pressure P , the travel S or the voltage U can be present many times for different cylinder

geometries and/or for values “g” defining the printing press status or the printing press, and can be appropriately selected, as depicted in [(]Fig. 9, as interrelationships C, D[)]].

[040] Such an interrelationship can also be advantageously used for starting and for running up the printing press to its operational speed, so that a suitable height for the raised area 09 is provided in connection with each roll-off speed “v.”

[041] In a further development, the regulating device permits an optimization of the actual production conditions or circumstances because[by means] of its adaptive structure.

[042] In case of the provision of a hydraulic unit, in accordance with the preferred[exemplary] embodiments in Figs. 4 to 7, a linearized interrelationship between the roll-off speed “v” and the reference value P_{sOLL} for the pressure P is stored as the logic, for example. A known interrelationship between the pressure P in the hollow body 11 and the resulting height h09 of the raised area 09 can be the basis for this logic. Now, the actuator 11, which is embodied as[as] a hollow

body 11₁ is charged with the appropriate pressure P , which is maintained, if required, by the use[means] of the regulator device 19, via the controlled system 22 which may be embodied as a valve 22, wherein an actual value P_{IST} is returned to the lower order regulating circuit. This[(this] accordingly applies to the manipulated values S , U , h_{09} , which differ from the pressure P [)]. Thus, the tongue/lip/bracket 09 is raised by the corresponding height h_{09} as a function of the roll-off speed " v " and in accordance with the existing pressure P_{IST} and is maintained there. If the roll-off speed " v ," or if another production condition, changes, the pressure P ₁ [(or one of the other manipulated values[])] is again determined and is again set. No continuous checking of the roll-off speed " v " need be performed. Instead[, instead], this can take place at[in] discrete intervals, for example following a fixed number of cylinder revolutions. In a further development, a starting value P_{IST} can also be supplied to the lower order regulating circuit, which can be predetermined from a printing press control, or also manually, for example during the start-up phase or under extremely non-stationary conditions.

[043] In a further preferred[exemplary] embodiment of the present invention, as shown in [(Fig. 10)], the reduction takes place by the use[means] of a higher order regulating device, which can again contain the previously[above] described regulating circuit of the lower order regulator device 19.

[044] In contrast to Fig. 8, in the embodiment depicted in Fig. 10, a value $e(t)$, which defines the cylinder on the press vibration, is fed₁ as the input value₁ to the logical unit 18. In particular, the value $e(t)$ contains a relative value between amplitudes a_1 , a_2 , which are measured at both cylinders 01, 02 and which are projected on a plane through the axes of rotation of the two cylinders 01, 02. Therefore, in what follows₁ the value $e(t)$ will also be called a relative amplitude $e(t)$. If the two cylinders 01, 02 vibrate equiphased in this plane₁ at the same amplitude $e(t)$, a resultant value of zero would result. In addition, as described in connection with Fig. 8, the roll- off speed "v" and/or other values "g" defining the printing press status or the printing press, can also be supplied as input values. In a further difference from[with] Fig. 8, in the embodiment depicted in Fig. 10, the logical unit 18 has an optimization algorithm which varies the output values

h_{09_SOLL} , P_{SOLL} on the basis of the values $e(t)$ in such a way that $e(t)$ is minimized.

[045] In an advantageous embodiment of the present invention, the variation takes place in accordance with[along] interrelationships which are stored in the logical unit 18, for example the dependence of the relative amplitude $e(t)$ on[from] the height h_{09} or on the pressure P , as shown in [(Fig. 11)], or on the distance a_{09} . It is possible to preset a group of curves or an arithmetic connection for different ranges of the roll-off speed " v " [(for example the number of revolutions)]. With the roll-off speed " v " [(or the number of revolutions)] known, a variation now takes place along the interrelationship preset for this roll-off speed " v " [(or this number of revolutions)]. For example, in Fig. 11 a curve identified by v_1 denotes a number of revolutions of 20,000 rph, v_2 of 40,000 rph, v_3 of 60,000 rph and v_4 of 80,000 rph. Here, too, a measurement of the vibrations and a variation possibly resulting therefrom need not take place continuously, but can be determined regularly within finite time intervals, or in accordance with a defined number of cylinder revolutions.

[046] Further processing of the reference variable h_{09_SOLL} , P_{SOLL} generated

in the logical unit in the described manner takes place in accordance with the process[way] explained in connection with Fig. 8.

[047] Fig. 12 shows a multi-roller system, and in particular a four-roller system, wherein the previously[already] described transfer cylinder 01 works or cooperates[does not only work] together with its forme cylinder 02, and also works,[but] in the contact position AN₁ with a further component 23, for example with a cylinder 23 configured as a counter-pressure cylinder 23, which, in this case, may be a second transfer cylinder 23. A component 24, for example a cylinder 24, for example a second forme cylinder 24, is assigned to the second transfer cylinder 23 and works together with the latter in the contact position AN. Only two of the four cylinders 01, 02, 23, 24, and in particular only the two transfer cylinders 01, 23, each have an actuator 11 and a raised area 09, whose height h₀₉ and/or whose phase relation or [(distance a₀₉)] can be changed. The principal functioning can also be applied to other multi-roller systems, such as to satellite units with 3, 9 or 10 cooperating cylinder, for example.

[048] Analogously to the preferred[exemplary] embodiment discussed in

accordance with Fig. 10, four amplitudes, or four vibration courses a_1, a_2, a_3, a_4 ,
and [(corresponding to the number of cylinders)], of the cylinders 01, 02, 23, 24
involved are determined, and from these amplitudes, [this] a number of relative
amplitudes $e_1(t), e_2(1), e_3(1)$, corresponding to the number of nip points, is
formed, which relative amplitudes are supplied, as input values, to the logical unit
18. Now, the optimization algorithm has an interrelationship for[per] each nip
point, for the respective passage of the raised area 09, or the interruption 06,
through the nip point. If one of the inner cylinders 01, 23, for example if the
transfer cylinder 01 is considered, the passage to the forme cylinder 02 at the nip
point takes place at a defined time, and the passage to the second transfer
cylinder 23 takes place at another defined time. Therefore, the demands made on
the optimal height h_{09} , or on the desired pressure P_{SOLL} , can be different for both
passages. It is now possible to resolve this problem advantageously in two
different ways.

[049] In a first preferred embodiment, a height $h_{09_{SOLL,1}}$, or a pressure
 $P_{SOLL,1}$ is determined in the logical unit 18 in such a way that a compromise is

found, while observing the two dependencies, taking into consideration the relative amplitudes $e_1(t)$, $e_2(t)$, which minimizes the two relative amplitudes $e_1(t)$, $e_2(1)$ as a whole. The same applies to the two other cylinders 23, 24, taking into consideration the relative amplitudes $e_3(t)$, $e_4(t)$ for the height $h_{09_{SOLL,2}}$, or the pressure $P_{SOLL,2}$. Then the respective actuator 11.1 or 11.2 is charged with the height h_{09} , or with the respective pressure P_1 , P_2 , which is or which will be regulated to $P_{SOLL,1}$ or to $P_{SOLL,2}$, corresponding to this compromise for the existing roll-off speed " v_r " via the associated regulating device 21.1, 21.2, and the controlled system 22.1, 22.2 which may be embodied as valves.

[050] In a second preferred embodiment, a phase-dependent variation of the optimization takes place for the height h_{09} , or for the pressure P_{SOLL} . It is now possible to change the height h_{09} of the raised area 09 at least twice for each[per] revolution of the cylinder 01, 23 using[with] the actuator 11, and in this case the raised area 09[it] assumes different values [respectively] at the times of its[the] passage through the one or the other respective nip points. Then the height h_{09} is changed for each[per] revolution as a function of the angular position of the

cylinder 01, 23 having the actuator 11. If more than one interruption 06 and/or more than one raised area 09 is arranged in the circumferential direction of the cylinder(s) 01, 02, 23, 24, the number of the possibly required changes, or the number of the values of the height h_{09} , possibly changes accordingly.

[051] In the case of the four cylinders 01, 02, 23, 24, two pressures $P_{SOLL,1}$, $P_{SOLL,2}$ are issued by the logical unit 18 as the reference variables $P_{SOLL,1}$, $P_{SOLL,2}$, each of which is fed into a lower order regulator device 19 of respective actuators 11 for[of] a changeable raised area 09. Here, the two raised areas 09 are arranged on the two transfer cylinders 01, 23.

[052] It is also possible to [respectively] arrange more than one raised area 09, for example to arrange two raised areas 09, in the circumferential direction. In this case, a common regulator device 19, as well as a common reference variable P_{SOLL} can be provided for each[per] raised area 09 of the cylinder 01, 02, 23, 24, and[but] also for all of the raised areas 09 of a cylinder 01, 23. Also, all cylinders 01, 02, 23, 24 can have raised areas 09 and/or interruptions 06.

[053] As explained above, in an advantageous embodiment of the present

invention, the distance a09, [(or the phase relation)], between the interruption 06 and the raised area 09 is also configured[designed] to be variable.

[054] In one preferred embodiment, this can take place, for example, mechanically wherein[in that] an effective shape of the raised area 09, or its absolute position, is changed. In the first case, an axially extending spindle, having the raised area 09, can have an appropriate shape on its exterior surface in such a way that, when turning the spindle by the use[means] of an actuator, which is not specifically represented, another area of the exterior of the spindle becomes effective as the raised area 09. In the second case, fingers, which are, for example, arranged in a comb-like manner on the surface area of the base body of the cylinder 01, 02, can be moved in the circumferential direction of the cylinder by an actuator, which is also not specifically represented.

[055] In another embodiment of the present invention, the two cooperating cylinders 01, 02, 23, 24 are embodied to be variable in their angle of rotation position φ with[phi in] respect to each other. In case the interruption 06 and the associated raised area 09 are arranged on different cylinders 01, 02, 23, 24, the

change in the relative angle of rotation position φ [phi] causes a change of the distance a09. For example, this can be realized in such a way that the two cylinders 01, 02, 23, 24 are rotatorily driven, mechanically independently of each other, by the use[means] of separate drive motors. In this case, one of the drive motors, which, as a rule, are electronically synchronized, is impressed with an offset in its reference angular position for changing the distance a09. However, the change of the relative angle of rotation position can also be performed by the use[means] of customary mechanical devices, such as are common, for example, for setting the position in the circumferential direction.

[056] The control, or the regulation, of the distance a09 can take place in a manner corresponding to the explanations of the preferred[exemplary] embodiments in accordance with Figs. 8 to 12. As explained in connection with the height h09, it is then possible to store appropriate interrelationships between the roll-off speed "v" and the distance a09, or to store optimization algorithms for accomplishing[creating] a variation of the distance a09 as a function of the relative amplitude e(t), and possibly of the roll-off speed "v."

[057] While preferred embodiments of a method and device for reducing vibrations on rotating parts, and vibration-damped rotating part, in accordance with the present invention have been set forth fully and completely hereinabove, it will be apparent to one of skill in the art that various changes in, for example, the overall sizes of the cylinders, the specific cylinder motors, and the like could be made without departing from the true spirit and scope of the present invention which is accordingly to be limited only by the appended claims.

WHAT IS CLAIMED IS:

[List of Reference Numerals]

- 01 Rotating component, cylinder, roller, transfer cylinder
- 02 Rotating component, cylinder, roller, forme cylinder
- 03 Surface area
- 04 Surface area
- 05 -
- 06 Interruption
- 07 Dressing, rubber blanket, printing forme, metal printing blanket
- 08 Groove, slit
- 09 Raised area, tongue/lip/bracket
- 10 Clamping and/or bracing device
- 11 Means for changing height, actuating means, actuator, hollow body
- 11.1 Means for changing height, actuating means, actuator, hollow body
- 11.2 Means for changing height, actuating means, actuator, hollow body
- 12 Groove
- 13 Interruption, cut, opening
- 14 Face
- 15 -
- 16 End, end of dressing (07)
- 17 End, end of dressing (07)
- 18 Logical unit
- 19 Regulator device
- 20 Lever mechanism
- 21 Regulating device, regulator
- 21.1 Regulating device, regulator]

- [21.2 Regulating device, regulator
- 22 Controlled system, valve
- 22.1 Controlled system, valve
- 22.2 Controlled system, valve
- 23 Component, cylinder, counter-pressure cylinder,
transfer cylinder
- 24 Component, cylinder, forme cylinder

- A Curve
- B Curve
- C Interrelationship
- D Interrelationship
- a09 Distance

- a1 Amplitude, course of vibration
- a2 Amplitude, course of vibration
- a3 Amplitude, course of vibration
- a4 Amplitude, course of vibration
- v1 Curve
- v2 Curve
- v3 Curve
- v4 Curve
- e(t) Value, relative amplitude
- e1(t) Value, relative amplitude
- e2(t) Value, relative amplitude
- e3(t) Value, relative amplitude
- phi Angle of rotation position

h09 Height (09)

h09_{IST} Reference variable

h09_{SOLL} Reference variable]

[h09_{SOLL.1} Reference variable

h09_{SOLL.2} Reference variable

l09 Effective leg length

P Pressure

P,1 Controlled system, valve

P,2 Controlled system, valve

P_{IST} Actual value

P_{SOLL} Reference variable

P_{SOLL.1} Reference variable

P_{SOLL.2} Reference variable

P_{SET} Set value

S Path, position

S_{IST} Reference variable

S_{SOLL} Reference variable

U Voltage

U_{SOLL} Reference variable

g Value

v Value, roll-off speed]